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# SHOCK TUBE STUDY OF NCO KINETICS

## MICHEL Y. LOUGE AND RONALD K. HANSON High Temperature Gasdynamics Laboratory

Department of Mechanical Engineering Stanford University Stanford, CA 94305

Mixtures of cyanogen, oxygen and nitrous oxide diluted in argon were shock-heated to measure the rate constant of:

$$NCO + O \rightarrow CO + NO.$$
 (3)

The primary diagnostic was narrow-line absorption of NCO at 440.479 nm using a remotely located cw ring dye laser source. A detailed kinetic analysis of the experiments near 1450° K led to:

$$k_3 = 10^{13.75 (-0.26, +0.20)} \text{ cm}^3/\text{mole/sec.}$$

Additional experiments, in mixtures of hydrogen cyanide, oxygen and nitrous oxide diluted in argon, enabled a determination of the ratio  $k_4/k_2$ :

$$C_2N_2 + O \rightarrow CN + NCO$$
 (2)

$$HCN + O \rightarrow NCO + H. \tag{4}$$

We found (at 1440° K):  $k_4/k_2 = 2.4$  (-0.9, +2.4). Utilizing a recent determination of  $k_2$ , we infer  $k_4 = 10^{11.70(-0.35, +0.40)}$  cm<sup>3</sup>/mole/sec.

### Introduction

Cyano species such as CN and NCO are known to play a key role in fuel-nitrogen chemistry<sup>1</sup> and the formation of combustion-generated nitric oxide. In an earlier paper on cyanogen oxidation kinetics,<sup>2</sup> we examined the conversion of  $C_2N_2$  to these cyano radicals. In this study, a novel laser absorption diagnostic was used to probe NCO time-histories in high temperature shock tube experiments aimed at determining rate constants for important NCO formation and removal reactions.

Mixtures of  $C_2N_2$ ,  $N_2O$  and  $O_2$  diluted in argon were shock-heated to determine the rate constant of reaction (3) at 1450° K, the rate constants for (1) and (2) being already well established:<sup>2</sup>

$$N_2O + M \rightarrow N_2 + O + M \tag{1}$$

 $C_2N_2 + O \rightarrow CN + NCO$  (2)

$$NCO + O \rightarrow CO + NO.$$
(3)

In other experiments,  $C_2N_2$  was replaced by HCN and a comparison of the NCO time-histories in the  $C_2N_2$  and HCN mixtures was used to establish a value for the rate of reaction (4) at 1440° K:

$$HCN + O \rightarrow NCO + H.$$
 (4)

There are no previous data for  $k_3$ , and data for  $k_4$  are limited. Roth *et al.*<sup>3</sup> measured  $k_4$  by shock heating HCN/N<sub>2</sub>O/Ar mixtures in the range 1800  $\leq T \leq 2500^{\circ}$  K and monitoring the H- and O-atom concentrations using an ARAS technique. Davies and Thrush<sup>4</sup> conducted a discharge flow study to find  $k_4$  in the range 469  $\leq T \leq 574^{\circ}$  K. Recently, Perry and Melius<sup>5</sup> obtained  $k_4$  in the range 540  $\leq T \leq 900^{\circ}$  K by monitoring NCO using a laser photolysis—laser induced fluorescence technique.

In this paper, the experimental facility and optical technique will first be described, then the data reduction and results for each of the mixtures will be presented.

#### Experimental

The experiments were conducted in a 15.24 cm internal diameter stainless-steel pressure-driven

shock tube.<sup>6</sup> Shock speeds varied between 1.14 and 1.17 mm/ $\mu$ sec, with attenuation of 1.5%/m or less. Typical leak plus outgassing rates were  $3 - 5 \times 10^{-5}$  torr/min. Gases were taken directly from commercial cylinders (Matheson) with the following purities:  $O_2$  and  $N_2O$  (>99.9%);  $C_2N_2$  (1.01% diluted in argon; HCN and CNCl < 50 ppmv,  $O_2 < 20$  ppmv,  $CO_2 < 20$  ppmv); HCN (Airco, 7.4% diluted in argon; H<sub>2</sub>O, SO<sub>2</sub>,  $O_2$  and  $CO_2 \le 1$  ppmv). The mole fraction of HCN in the cylinder was checked against known  $C_2N_2$  and HCN mixtures using high-temperature CN emission tests since HCN may slowly decompose in high pressure cylinders.

The shock tube test section and laser absorption system for NCO are shown schematically in Fig. 1. The signal obtained from the double-pass NCO diagnostic was recorded on a digital oscilloscope (Nicolet Explorer III, dc-coupled through a 100 kHz upper frequency cut-off filter) and stored on tape for subsequent data reduction.

The absorption from the  $P_2 + {}^PQ_{12}$  band head of the  $[A^2\Sigma^*(00^00) \leftarrow X^2\Pi_i(00^10)]$  band of NCO at 440.479 nm (vac.) was used to monitor NCO. The laser system consisted of a UV-enhanced Ar\* laser (Spectra Physics model 171-18) and a standard Spectra Physics 380A ring dye laser. The available Ar<sup>+</sup> UV power (1.9 W all lines) was sufficient to excite the stilbene S3 dye above threshold, providing a typical dye laser output power of 60 mW. The nominal laser wavelength was varied using a standard 3-plate birefringent filter; fine tuning was achieved with an uncoated 5 mm-thick fused silica etalon in a temperature-controlled oven. Single mode output of the laser was verified using a confocal interferometer (Spectra Physics model 470, free spectral range 2 GHz). An amplitude stabilizer (Coherent Associates model 307) was employed to improve the signal quality. The component of the laser power



FIG. 1. Shock tube NCO laser absorption diagnostic.

rejected by the amplitude stabilizer was sufficient to drive the wavemeter (Burleigh model WA-10) used for setting the laser wavelength. It was necessary to correct the displayed wavelength for the change in the index of refraction of air between the He-Ne reference wavelength at 632.991 nm and our blue wavelength at 440.479 nm (correction = actual - displayed wavelength =  $\pm 0.002$  nm).

The laser light was coupled into a 200 µm fused silica optical fiber for transport to the shock tube facility<sup>7</sup> (length: 65 m). The output from the optical fiber was double-passed through the shock tube test section as shown in Fig. 1. The incident and return beams were monitored on two separate detectors D1 and D2 (EG&C UV 100B silicon photodiodes mounted in an amplifier/filter package with a 240 kHz (-3dB) cutoff frequency). Neutral density filters (transmission:  $10^{-1}$ ) were used to reduce the incident power of 1 mW below the saturation limit of the detectors while proportionally reducing the spontaneous emission from the test gas. Narrow bandpass filters (FWHM: 40 nm, centered at 450 nm) were used to discriminate against other sources (primarily room lights). The signal from each detector was passed through a differential amplifier (Tektronix model AM 502, dc-1MHz bandwidth). Prior to each experiment, the laser light was chopped to balance (i.e., equalize) the reference signal  $(i_0)$ and the return signal (i) using small dc offset and gain adjustments on one of the differential amplifiers. The difference  $(i_0 - i)$  and the reference signal  $(i_0)$  were recorded on two separate oscilloscope channels, thereby providing a direct measurement of the fractional absorption through the system.

Three runs were conducted with the following mixtures and conditions:  $N_2O:O_2:C_2N_2:Ar =$ 4:1:4:991,  $T_2 = 1450 \pm 10^\circ$  K,  $P_2 = 0.60$  atm, and  $\rho_{21} = 3.31$  ( $\rho_{21}$  is the density ratio across the shock and also the ratio of particle time to laboratory time). Nine additional runs were conducted with HCN mixtures:  $N_2O:O_2:HCN:Ar = 8:1:8:983$ ,  $T_2 = 1430$  $\pm 20^\circ$  K,  $P_2 = 0.60$  atm, and  $\rho_{21} = 3.32$ . The temperature of the experiments was set by considerations of growing interference on NCO removal by reaction (5) at higher temperatures.

$$NCO + M \rightarrow N + CO + M \tag{5}$$

and diminishing confidence in the rate of reaction (1) at lower temperatures. In addition, a few tests were conducted with the laser blocked to monitor possible spontaneous emission interferences from the test gas. These emission levels were found to be insignificant.

The transmission of the laser system is related to the level of NCO through the Lambert-Beer law:

$$\frac{i}{i_0} = \exp[-\beta(\lambda) p_{\rm NCO} L]$$

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where  $i/i_0$  is the fractional transmission,  $\beta(\lambda)$  is the absorption coefficient at wavelength  $\lambda$ ,  $p_{NCO}$  is the partial pressure of NCO and L is the optical path length (30.5 cm). The data reduction procedure was based on relative profiles of NCO concentrations and hence did not require knowledge of  $\beta$ ; however,  $\beta$ has been determined recently in our laboratory.<sup>8</sup>

In order to establish the optimum wavelength for NCO detection, the relative absorption coefficient was measured as a function of wavelength by conducting nine nearly identical HCN experiments (see above), each at a different laser wavelength. The relative absorption coefficient (corrected for small excursions in the shock wave conditions) is plotted along with a computer-predicted profile in Fig. 2. The peak of the absorption coefficient was measured to be near 440.479 nm, in good agreement with our expectations and the value quoted by Dixon.<sup>9</sup>

### N<sub>2</sub>O/O<sub>2</sub>/C<sub>2</sub>N<sub>2</sub>/Ar Mixtures—Analysis and Results

# a) Reaction Mechanism:

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A complete reaction mechanism was utilized in the data reduction (see Table I), but a simplified description can be given as follows. At early times,  $N_2O$  rapidly decomposes to provide O-atoms;  $C_2N_2$ then reacts to form NCO, which in turn is removed by O-atoms:



Fig. 2. NCO absorption spectrum around 440.479 nm. The horizontal error bars on the experimental data correspond to the wavemeter resolution. The solid line is based on a spectroscopic model, including 30 lines near the  $P_2$  +  ${}^{P}Q_{12}$  band head and assuming a Voigt "a" parameter of 0.1.<sup>8</sup>

$$N_2O + M \rightarrow N_2 + O + M \tag{1}$$

$$C_2N_2 + O \rightarrow CN + NCO$$
 (2)

$$NCO + O \rightarrow CO + NO.$$
 (3)

The presence of molecular oxygen converts the CN into additional NCO and replenishes the O-atom pool via reaction (6):

$$CN + O_2 \rightarrow NCO + O_2$$
 (6)

Assuming a steady-state of [CN] between reaction (2) and (6), the rate of change of NCO concentration is given by:

$$\frac{d[\text{NCO}]}{dt} = 2 k_2 [C_2 N_2] [O] - k_3 [\text{NCO}] [O].$$

Since O and  $C_2N_2$  are nearly constant throughout the process (see Fig. 3), the NCO profile eventually reaches a plateau (d[NCO]/dt = O) where

$$\frac{[\text{NCO}]^{\text{plateau}}}{[\text{C}_2\text{N}_2]} \simeq \frac{2 k_2}{k_3}.$$

It follows that the relative NCO profile (using the plateau as a reference) depends primarily on the rate of reaction (3), since (for this simplified model):

$$\frac{d[\text{NCO}]/[\text{NCO}]^{\text{plateau}}}{dt} \approx k_3[\text{O}] (1 - [\text{NCO}]/[\text{NCO}]^{\text{plateau}}).$$

The NCO plateau concentration thus depends primarily on the ratio  $k_2/k_3$  and the relative time behavior depends on  $k_3$ . An absorption record of NCO is therefore sufficient to infer  $k_3$  and, using the established value of  $k_2$ ,<sup>2</sup> the absolute value for the NCO plateau concentration. This approach for the establishment of a known level of NCO was utilized in a recent study of NCO spectroscopy.<sup>8</sup>

Vibrational equilibrium of NCO was assumed, even though there is some evidence for NCO production in excited vibrational states from reaction (6) at lower temperatures.<sup>10</sup>

# b) Results and Discussion:

A numerical routine derived from the NASA-Lewis general chemical kinetics program, <sup>19</sup> and incorporating the mechanism in Table I, was used for the kinetics calculations. Values for  $k_3$  were inferred from best fits to the measured relative NCO concentration profiles. Figure 4 shows such a best fit (solid line) to the relative NCO trace and the influence of varying  $k_3$  using factors of 0.67 and 1.50

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Repotions		equil. const. <sup>b</sup>	rate constants			- Eau
Neactions	ΔH•		log <sub>10</sub> A	m	θ(°K)	(Ref #)
$1 N_2O + M \rightarrow N_2 + O + M$ $2 C_1N_2 + O \rightarrow CN + NCO$ $3 NCO + O \rightarrow NO + CO$ $4 HCN + O \rightarrow NCO + H$ $5 NCO + M \rightarrow N + CO + M$ $6 CN + O_2 \rightarrow NCO + O$ $7 CN + O \rightarrow CO (v = 1) + N$ $8 NCO + H \rightarrow CO + NH$ $9 HCN + O \rightarrow NH + CO$ $10 HCN + OH \rightarrow H_2O + CN$ $11 N_2O + O \rightarrow NO + NO$ $12 N_2O + O \rightarrow N + NO$ $12 N_2O + O \rightarrow N + NO$ $14 NO + O \rightarrow N + O_2$ $15 NCO + N \rightarrow N_2 + CO$ $16 NCO + N \rightarrow CN + NO$ $17 NCO + OH \rightarrow HNCO + O$	$ \Delta H^{*} $ +40 +4 -105 0 +48 -2 -69 -39 -39 -39 +1 -38 -81 +75 +32 -180 -30 -19	$\begin{array}{c} \text{const.}^{\text{b}} \\ -3.8 \\ 0.3 \\ 15.4 \\ -0.4 \\ -5.8 \\ 0.1 \\ 9.2 \\ 6.0 \\ 5.6 \\ -0.2 \\ 7.1 \\ 12.1 \\ -10.3 \\ -5.3 \\ 25.7 \\ 5.2 \\ 0.9 \end{array}$	log10A 23.89 12.66 13.75 8.24 16.80 12.75 13.31 14.02 8.73 12.64 13.84 14.00 14.26 9.58 13.30 14.66	m -2.5 0 0 1.47 -0.5 0 0 0 1.21 0 0 0 0 0 0 1.0 0 0	θ(°K) 32710 4440 0 3775 24000 0 210 1000 3825 4530 13400 14100 38370 20820 0 5530	(Ref #) [11] [2] This study [12] [2] [2] [2] [12] [13] [11] [11] [11] [11] [11] [11] [11] [12]
$18 N_2O + H \rightarrow N_2 + OH$ $19 O_2 + H \rightarrow OH + O$ $20 H_2 + O \rightarrow H + OH$	-65 +16 +2	10.8 -1.2 +0.1	13.30 13.88 17.57	0 0 -1.0	0 7600 8810	estimate [11] [16]
$21 H_2O + O \rightarrow OH + OH$ $22 OH + H_2 \rightarrow H + H_2O$ $23 CN + H_2 \rightarrow HCN + H$ $24 CN + HCN \rightarrow C_2N_2 + H$ $25 NH + O \rightarrow NO + H$ $26 NH + H \rightarrow N + H$	+17 -15 -16 -4 -66	-1.5 1.6 1.8 -0.7 9.4	9.66 9.07 11.74 13.30 11.80	1.0 1.3 1.3 0.7 0 0.5	4480 8605 1825 2460 2140 0	[16] [16] [17] [13] [12]*
	-20	2.7	13.70	0	1000	

"Heat of reaction at 1500" K (kcal/mole).<sup>18</sup> We used  $\Delta Hf_0^{\circ}(CN) = 101$  kcal/mole, an average of the values of Janaf<sup>18</sup> and Colket.<sup>21</sup>

 $b\log_{10} (k_{\text{forward}}/k_{\text{backward}})$  at 1500° K.

**T**].

"Using the notation  $k = A T^{m} \exp[-\theta/T]$  (cm<sup>3</sup>/mole/sec).

Colket measured  $k_{\text{backward}} = 10^{14} \exp[-21190/T]$  (cm<sup>3</sup>/mole/sec); we assumed  $k_f/k_b = 4.54 \exp[15660/cm^2]$ T]. We measured  $k_{backward} = 10^{14.5} \exp[-4030/T]$  (cm<sup>3</sup>/mole/sec); we assumed  $k_f/k_b = 0.058 \exp[1890/\frac{1}{2}]$ 

(dashed lines). The modified curves clearly fail to fit the data. We conservatively estimate the range of possible values for an acceptable fit to be  $[\times 0.74,$ ×1.35] around the reported rate. Additional uncertainties in k3 may result from uncertain knowledge of other rates of reactions present in the mechanism. In order to estimate these uncertainties, individual rates (Table I) were adjusted by reasonable factors (based on current literature or our judgment);  $k_3$  was subsequently modified to ensure the return to an optimum fit. We found the resulting uncertainty in  $k_3$  to be approximately [×0.60, ×1.42]. The two uncorrelated uncertainties mentioned above may be combined to give a global uncertainty of  $[\Sigma(\text{uncertainty})^2]^{1/2} \approx [\times 0.55, \times 1.60].$ 

On the basis of this analysis, we recommend a temperatures near 1450° K:

$$k_3 = 10^{13.75(-0.26, +0.20)}$$
 cm<sup>3</sup>/mole/sec.

There are no previous data available for comparison.

From the computer-predicted NCO plateau and the corresponding experimental absorption, we can infer a value for  $\beta$ , the absorption coefficient at the peak wavelength. Uncertainties in  $\beta$  include experimental scatter, uncertainty in the Voigt parameter "a," and the uncertain knowledge of some reaction rates, including  $k_2$  and  $k_3$ . For a typical experiment, with an absorption plateau of 5% and

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-	Source (Ref #)			
0 40 0 75 00 210 000 925 530 400 100 370 320 0 300 10 80 05 25 60 40 0 20 25 500 10 20 20 20 20 20 20 20 20 20 2	[11] [2] This study [12] [2] [2] [2] [13] [11] [11] [11] [11] [11] [11] [14] [15] <sup>4</sup> estimate [11] [16] [16] [16] [17] [13] [12] <sup>*</sup> [11]			
an average of the				

= 4.54 exp[15660/

\* 0.058 exp[1890/

we recommend at

1<sup>3</sup>/mole/sec.

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NCO plateau and absorption, we can a coefficient at the in  $\beta$  include exthe Voigt paramledge of some re $k_3$ . For a typical plateau of 5% and



FIG. 3. Computer-generated profiles of N<sub>2</sub>O, C<sub>2</sub>N<sub>2</sub>, O<sub>2</sub>, NCO, O, CN and N mole fractions using the rates shown in Table I. Conditions: T<sub>2</sub> = 1440° K,  $p_2 = 0.60$  atm, N<sub>2</sub>O:O<sub>2</sub>:C<sub>2</sub>N<sub>2</sub>:Ar = 4:1:4:991 and  $p_{21}$ = 3.31.

 $p_{\rm NCO} \simeq 0.012$  torr  $(p_{\rm NCO}/p \simeq 26$  ppmv), we have:<sup>8</sup>  $\beta(1450^{\circ} \text{ K}) \simeq 110 (-50, +130) \text{ cm}^{-1} \text{ atm}^{-1}$ at 440.479 nm.

The signal-to-noise ratio achieved in these experiments was about 30, so that the detection limit of NCO (S/N = 1) using this scheme is about 1 ppmv.

### N<sub>2</sub>O/O<sub>2</sub>/HCN/Ar Mixtures—Analysis and Results

Data from these experiments were reduced using the complete kinetic mechanism in Table I, but a simplified model based on the following reactions is helpful in appreciating the similarity between the  $C_2N_2$  and HCN experiments:

 $N_2O + M \rightarrow N_2 + O + M \tag{1}$ 

$$HCN + O \rightarrow NCO + H$$
 (4)

$$NCO + O \rightarrow NO + CO$$
 (3)

$$NCO + H \rightarrow NH + CO.$$
 (8)

As with the  $C_2N_2$  mixtures, the relative NCO trace depends on the rate of NCO removal  $k_3[O] + k_8[H]$ , and the plateau NCO concentration (normalized by the concentration of the NCO source, i.e. [HCN]) is given approximately by the ratio of the rate constants for the formation and removal steps:



FIG. 4. Best computer fit to a typical experimental trace. Conditions:  $T_2 = 1440^{\circ}$  K,  $p_2 = 0.60$  atm and  $N_2O:O_2:C_2N_2:Ar = 4:1:4:991$ . Abscissa: Laboratory time (microseconds). Absorption at 500 µsec = 4.6%. Solid line: best computer fit using  $k_3 =$  $10^{13.75}$  cm<sup>3</sup>/mole/sec and other rates shown in Table I. Dotted lines: Computer-generated profile using best rates, except: —  $k_3$  [×1.50] and …  $k_3$ [×0.67].

$$\frac{[\text{NCO]}^{\text{plateau}}}{[\text{HCN}]} \approx \frac{k_4}{k_3 + k_8} \frac{[\text{H}]}{[\text{O}]}$$

Values of the steady-state concentrations of H- and O-atoms can be computed using the complete mechanism in Table I. Under typical conditions for the HCN mixtures, we have  $[H]/[O] \approx 1.6$ .

By conducting HCN and  $C_2N_2$  experiments under similar conditions of temperature and pressure, it is therefore possible to infer the ratio  $k_4/k_2$  by comparing the respective NCO absorption plateaus. We have:

$$\frac{[\text{NCO}]^{\text{plateau}}/[\text{HCN}]}{[\text{NCO}]^{\text{plateau}}/[\text{C}_2\text{N}_2]} \approx \frac{k_4}{2 k_2} \times \frac{1}{1 + \frac{k_8}{k_3} \times \frac{[\text{H}]}{[\text{O}]}}$$

This approach makes the measurement of  $k_4/k_2$  independent of the uncertainties associated with  $\beta$  that we reported above. However, the uncertain knowledge of some reaction rates in the mechanism (including  $k_3$  and  $k_6$ ) introduces an uncertainty of [ $\times 0.6$ ,  $\times 2.0$ ] in the ratio. (Note that the rate of reaction (8) has been recently determined at 1490° K in our laboratory.<sup>12</sup>) A reduction of the overall un-

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FIC. 5. Arrhenius plot for  $k_4$ .

certainty in  $k_4/k_2$  could be achieved with further optimization of reactant mixtures.

We found at temperatures near 1440° K:  $k_4/k_2$ = 2.4 (-0.9, +2.4). Using our previously reported value<sup>2</sup> for  $k_2 \approx 10^{12.66} \exp[-4440/T] \text{ cm}^3/\text{mole}/$ sec [×0.54, ×1.86], we calculate  $k_4 =$  $10^{11.76(-0.35, +0.40)} \text{ cm}^3/\text{mole}/\text{sec}$  at 1440° K. This determination of  $k_4$  is plotted in Fig. 5 along with the earlier results of Roth *et al.*<sup>3</sup> and Davies and Thrush,<sup>4</sup> and the recent data of Perry and Melius.<sup>5</sup>

Melius and Binkley<sup>20</sup> recently showed that the reaction of HCN with O atoms follows two major path:



$$\rightarrow \begin{cases} \text{NCO} + \text{H} & (4) \\ (\text{HNCO})^{t} \rightarrow \text{NH} + \text{CO}. & (9) \end{cases}$$

Using transition state theory, and the results of Melius and Binkley,<sup>20</sup> Perry and Melius<sup>5</sup> calculated the temperature dependence of  $k_4$ :

$$k_4 \propto T^{1.47} \exp[-3775/T].$$

This temperature dependence is in excellent agreement with the three independent studies of Roth, et al.,<sup>3</sup> Perry and Melius,<sup>5</sup> and this study. For the purpose of providing a single expression for use over the temperature range  $540 \le T \le 2500^{\circ}$  K, we have assumed the temperature dependence calculated by Perry and Melius<sup>5</sup> and computed a leastsquares fit expression based on the two end points of Roth et al., the two end points of Perry and Melius, and one point from this study. On the basis of this analysis, we recommend  $k_4 = 10^{8.24} T^{1.47} \exp[-3775/T] \text{ cm}^3/\text{mole/sec} (\pm 30\%)$  in the range  $540 \le T \le 2500^{\circ} \text{ K}.$ 

It should be noted that this expression does not extrapolate well into the temperature range studied by Davies and Thrush.<sup>4</sup> Our recommended expression is lower than their value by about 50%. However, the value reported by Davies and Thrush should be interpreted as a total reaction rate  $(k_4 + k_9)$  (despite their assumption that NCO and H are the most likely products of this reaction), since they did not treat reaction (4) as a specific path for the (HCN + O) reaction. Thus, the results of Davies and Thrush are in excellent agreement with the total rate  $(k_4 + k_9)$  of Perry and Melius, who found  $k_9/k_4 = 0.5.^5$ 

### Acknowledgments

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W. J. McLean, Sandia National Laboratories, USA.

Your results are affected by uncertainties in rate constants used in the model as well as by experi-

mental uncertainties. Are you able to ascertain the

contributions of such rate constant uncertainties to

Authors' Reply. Uncertainties in the rate mea-

surements do result from the uncertain knowledge

of other rates of reactions present in the mecha-

nism. In order to estimate these uncertainties, in-

dividual rates (Table 1) were adjusted by reasonable

factors (based on current literature or our judg-

ment); values of the rate measurements were sub-

sequently modified to ensure the return to an op-

timal fit. Using a linear statistical analysis of these

uncorrelated individual uncertainties, we estimated

the total uncertainty on a rate measurement to be

total uncertainty =  $[\Sigma(\text{uncertainty})^2]^{1/2}$ .

D. M. Golden, SRI International, USA. What evi-

dence is there that the reaction O + HCN is pres-

sure independent? If the experiments do show pressure independence, is this what would be ex-

pected from the Melius surface and an RRKM life-

Authors' Reply. The pressure range of our ex-

periments is too narrow to assess the effect of pres-

your overall uncertainty?

given by

time calculation?

sure on the rate of reaction (4)

hensive Chemical Kinetics, 17, 1, (C. H. Bamford and C. F. H. Tipper, Editors), Elsevier, Amsterdam.

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# COMMENTS

 $HCN + O \rightarrow NCO + H.$  (4)

Please refer to Robert Perry's question for additional comments about this reaction.

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R. A. Perry, Sandia National Laboratories, USA. In the analysis of the kinetics of the reaction of  $O(^{\circ}p)$  + HCN  $\rightarrow$  NCO + H a detailed knowledge of the relative concentrations of H and O atoms is required. How sensitive is your calculated rate coefficient to the calculated H and O atom concentrations? What are the estimated concentrations associated with these estimates?

In response to David Golden's questions, a similar question was asked by Van Tiggelen to myself about my paper at this symposium. While the calculations did not address this question directly the fact that the energy barriers for rearrangement to form NH + CO and simple bond fission to form NCO + H are nearly equivalent argues against a major pressure dependence on the products. Also, no pressure dependence is observed for the total rate from low pressures torr to 200 torr total pressure.

Authors' Reply. As indicated in the text, the ratio  $k_4/k_2$  was inferred by comparing the steady-state NCO concentrations in the HCN and  $C_2N_2$  mixtures. The data reduction was performed on the computer using a multi-reaction model based on the mechanism of Table 1. However, a simplified model is helpful in understanding the data reduction.pro-

#### **REACTION KINETICS**

(8)

cedure and the sensitivity of the present measurement of  $k_4/k_2$  to the rate of reaction (8),

$$NCO + H \rightarrow NH + CO$$

Using this simplified model,

$$\frac{[\mathrm{NCO}]^{\mathrm{plateau}}/[\mathrm{HCN}]}{[\mathrm{NCO}]^{\mathrm{plateau}}/[\mathrm{C}_2\mathrm{N}_2]} \approx \frac{k_4}{2 k_2} \times \frac{1}{1 + \frac{k_6 [\mathrm{H}]}{k_3 [\mathrm{O}]}}.$$

Thus, the extraction of  $k_4/k_2$  from the experimental ratio of NCO concentrations requires the knowledge of [H]/[O] and  $k_a/k_3$ . Values of the steadystate H- and O-atoms concentrations can be computed using the complete mechanism in Table 1. Under the present conditions [H]/[O]  $\approx$  1.6. In addition,  $k_3$  and  $k_a$  have been measured in our laboratory, with the results  $k_3 = 10^{13.73}$  cm<sup>3</sup>/mole/sec at 1450° K and  $k_a = 10^{13.73}$  cm<sup>3</sup>/mole/sec at 1490° K.<sup>12</sup> Note that the uncertainty analysis reported in the present paper was based on the complete mechanism of Table 1: the sensitivity of  $k_4/k_2$  to uncertainties in [H], [O],  $k_3$ ,  $k_8$  and other rates was estimated using this mechanism.

Thank you for your comments regarding Dr. Golden's question.

C. F. Melius, Sandia National Laboratories, USA. Have you considered the branching ratio of O + NCO to form  $N + CO_2$  compared to NO + CO and could it be important in the formation of N atoms from fuel-bound nitrogen?

Authors' Reply. In these experiments, the direct measurement of NCO makes the determination of the rate of the reaction

NCO + O  $\rightarrow$  products, (3)

fairly insensitive to the composition of the products. Nevertheless, we have assumed in the data reduction that the products of reaction (3) are NO + CO,

$$NCO + O \rightarrow NO + CO$$
, (3a)

rather than N + CO<sub>2</sub>,

$$NCO + O \rightarrow CO_2 + N.$$
 (3b)

If reaction (3b) proves a significant branching of reaction (3), then the NCO  $\rightarrow$  NH  $\rightarrow$  N sequence of the fuel-nitrogen mechanism may be partially bypassed by reaction (3b). Thus, further theoretical or experimental work is needed to assess the magnitude of the possible branching ratios of reaction (3).

A. Lifshitz, Hebrew University of Jerusalem, Israel. Did you consider the termination reaction:  $2NCO \rightarrow N_2 + 2CO$ ? Also, did you consider the reaction:  $NCO + O_2 \rightarrow NO + CO + O$ ? Without the  $NCO + O_2$  reaction we could not fit our computed ignition delay times to the experimental ones in shock heated mixtures of  $C_2N_2 + O_2 + Ar$  and  $C_2N_2 + O_2 + H_2 + Ar$ . We believe that this reaction does exist. The rate constant that we have assigned to this reaction is:  $1.6 \times 10^{13} \exp (-19000/$ RT) cc mole<sup>-1</sup>sec<sup>-1</sup>.

Authors' Reply. Despite its high exothermicity  $(\Delta H_R \simeq -137 \text{ kcal/mole at } 1500^\circ \text{ K})$ , the reaction

$$NCO + NCO \rightarrow N_2 + CO + CO$$
 (a)

was not considered in the present data reduction, because the path to  $N_2$  + 2CO requires a complex rearrangement of molecular bonds, with a presumably low transition probability.

Using similar arguments, the endothermic reaction

$$NCO + O_2 \rightarrow NO + CO + O$$
 (b)

can be omitted from the present study of dilute  $C_2N_2/O_2/N_2O$ /argon mixtures ( $\Delta H_R \approx +16$  kcal/mole at 1500° K). In addition, according to your evaluation  $k_b = 1.6 \ 10^{13} \ \exp[-19000/\text{RT}] \ \text{cm}^3/\text{mole/sec}$ , the rate of reaction (b) is about seven times slower than the rate of reaction (3)

$$NCO + O \rightarrow NO + CO$$
, (3)

under the present experimental conditions (T = 1500° K). Thus, reaction (b) constitutes only a minor interference to the data reduction leading to  $k_3$ .