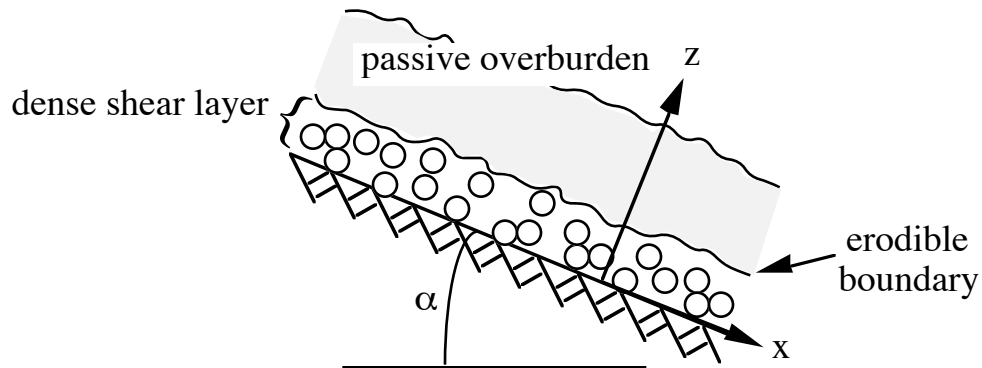


Hydraulic Model - Dense Flows

mass holdup H^\dagger , mean velocity \bar{u} and volume fraction \bar{v} , gravity g , inclination α , grain diameter D , effective friction μ_{eff}



Mass and momentum balances

$$\frac{\partial H^\dagger}{\partial t} + \frac{\partial(\bar{u} H^\dagger)}{\partial x} = 0$$

$$\frac{\partial \bar{u}}{\partial t} + \bar{u} \frac{\partial \bar{u}}{\partial x} + \frac{g D \cos \alpha}{\bar{v}} \frac{\partial H^\dagger}{\partial x} = g \cos \alpha (\tan \alpha - \mu_{\text{eff}})$$

Calculate μ_{eff} from local balance equations

Local solution

mass holdup H^\dagger , basal volume fraction v_0 , temperature T_0 , and velocity u_0
 enduring friction μ_E , impulsive friction μ_I , normal restitution e_I

Equations at the base

Shear stress: $S = S_I + S_E$

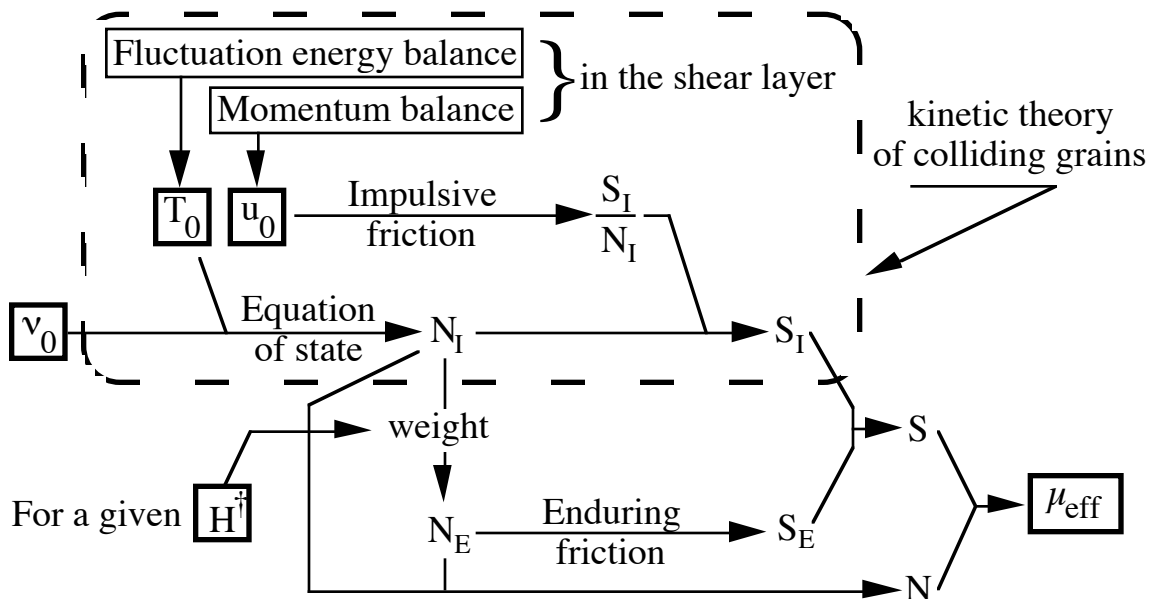
Weight: $N = N_I + N_E = \rho_s g D H^\dagger \cos \alpha$

Enduring friction: $S_E/N_E = \mu_E$

Impulsive friction: $S_I/N_I = f(u_0/\sqrt{3T_0})$

Equation of state: $N_I = (1/2) \rho_s v_0 g_{12}(v_0) (1+e_I) T_0$

Solution procedure



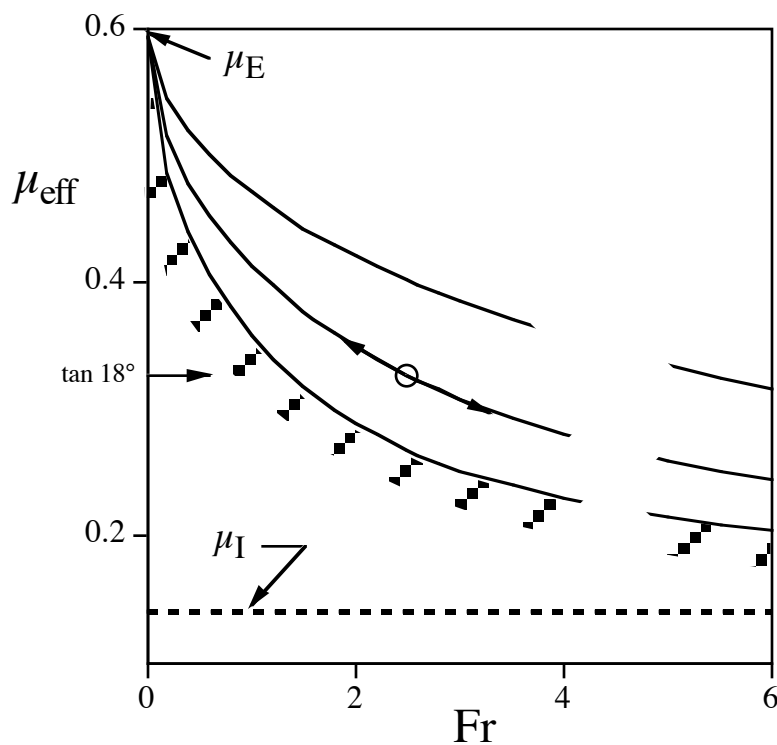
It remains to evaluate v_0 .

Effective friction

$$\mu_{\text{eff}} = \mu_E - v_0 g_{12}(v_0) \frac{(1+e_I)}{2} \frac{(\mu_E - S_I/N_I)}{h} \text{Fr}^2$$

with

$$\text{Fr} \equiv \frac{\bar{u}/\sqrt{gD}}{\sqrt{H^\dagger \cos \alpha}} \quad \text{and} \quad h \equiv \bar{u}^2 / T_0$$



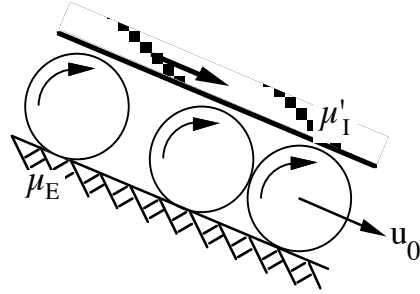
Collisions “lubricate” the flow.

*If v_0 stayed constant,
then the flow would be unstable.*

Closure of v_0 - Angular momentum balance

At steady-state, the flow adjusts v_0 to balance
production $\mathbb{P}(\omega)$ = dissipation $\mathbb{D}(\omega)$

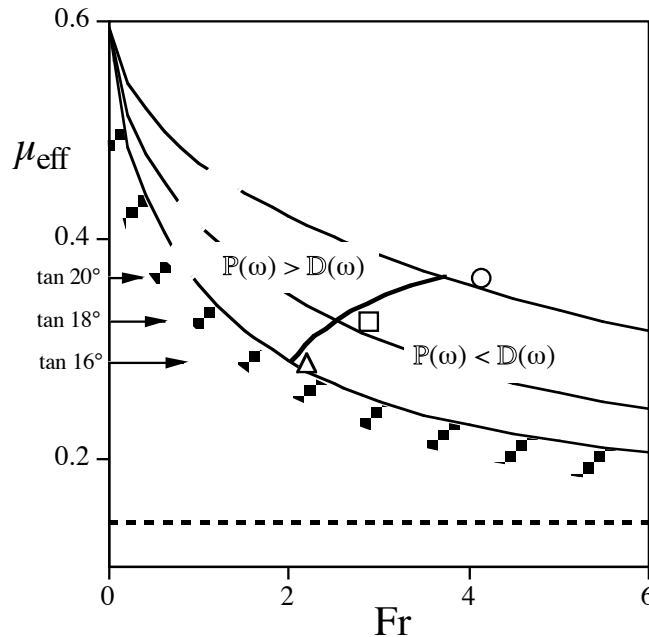
$$\mathbb{P} = (5 g \cos \alpha / D) [(H/D) (\mu_E + \mu'_I) - \mu'_I]$$



Collisions among spheres touching the base

$$\Delta\omega = - (5/2D) (1+e'_I) \mu'_I u_0 \quad \text{at a frequency} \sim u_0 / (D\pi/6v_0)$$

$$\Rightarrow \mathbb{D} \sim (5/2D^2) (1+e'_I) \mu'^2_I u_0^2 (6v_0 / \pi)$$



The balance stabilizes the flow.